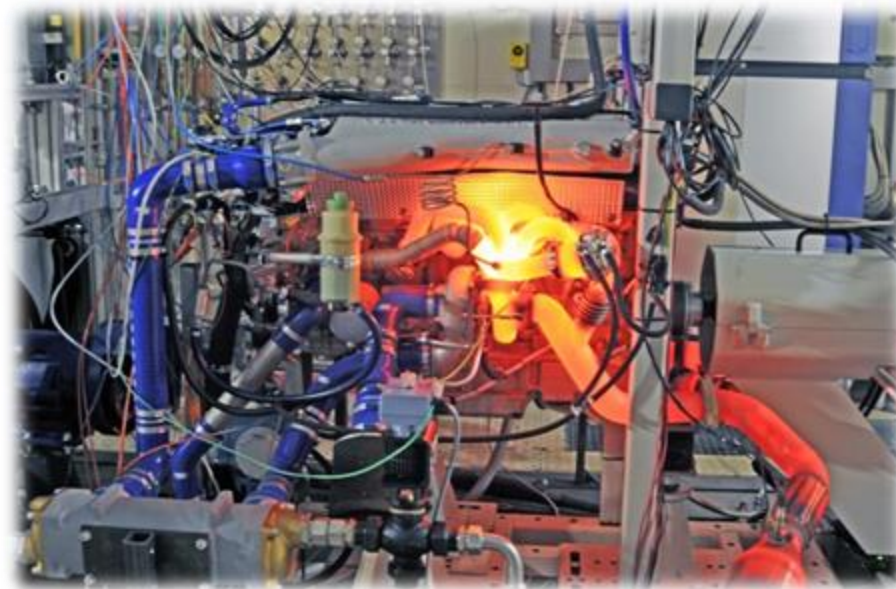


More than just the past: Perspectives of future combustion engines as sustainable drive systems

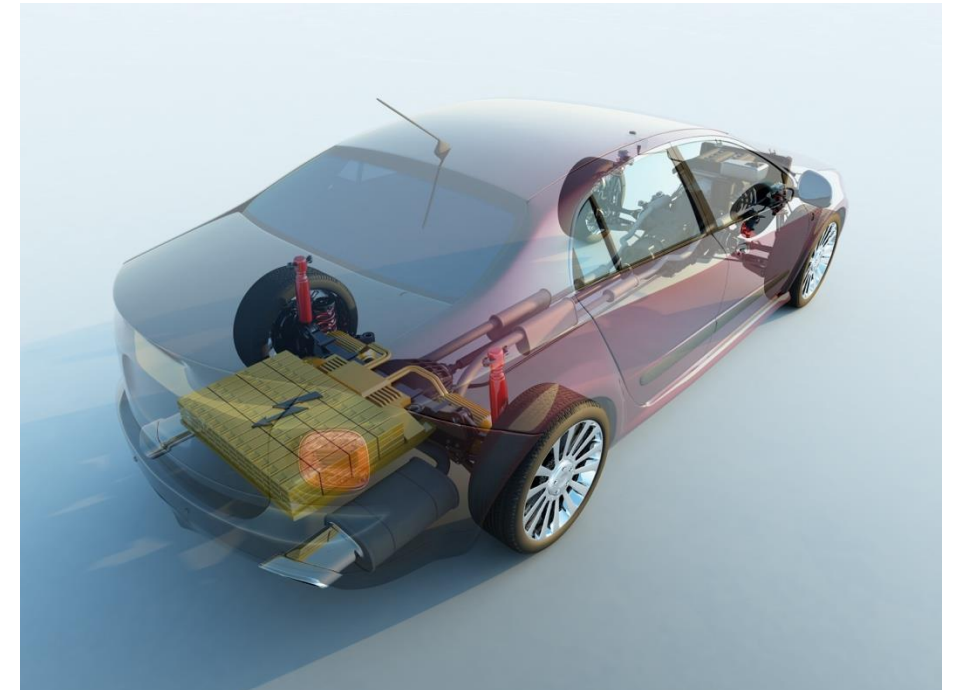


Univ.-Prof. Dr.-techn. Helmut Eichlseder, Univ.-Prof. Dr.-Ing. Christian Trapp

More than just the past:

Perspectives of future combustion engines as sustainable drive systems

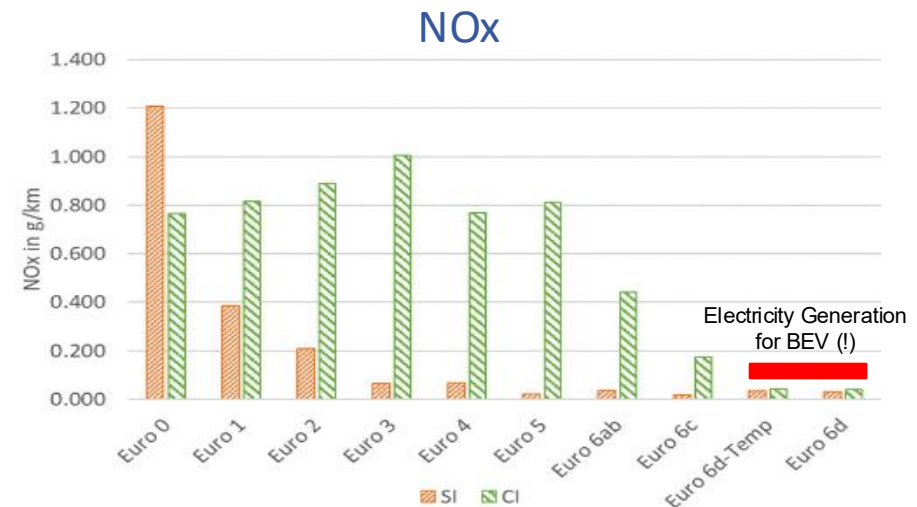
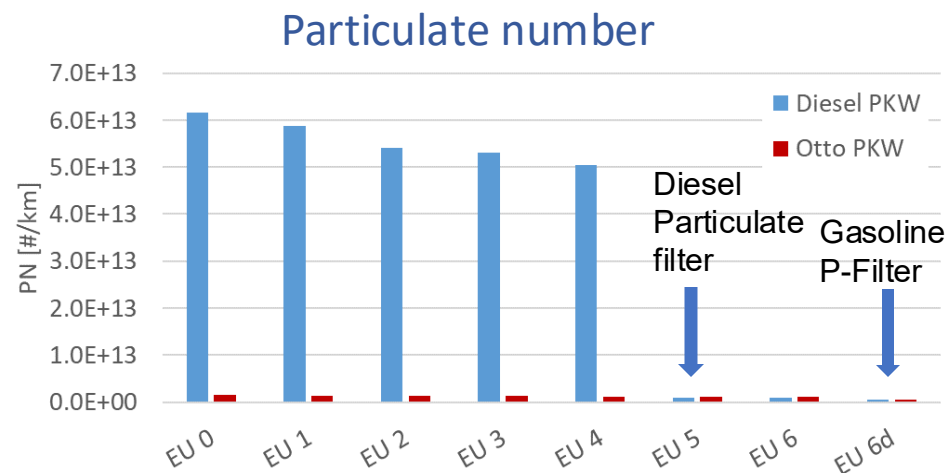
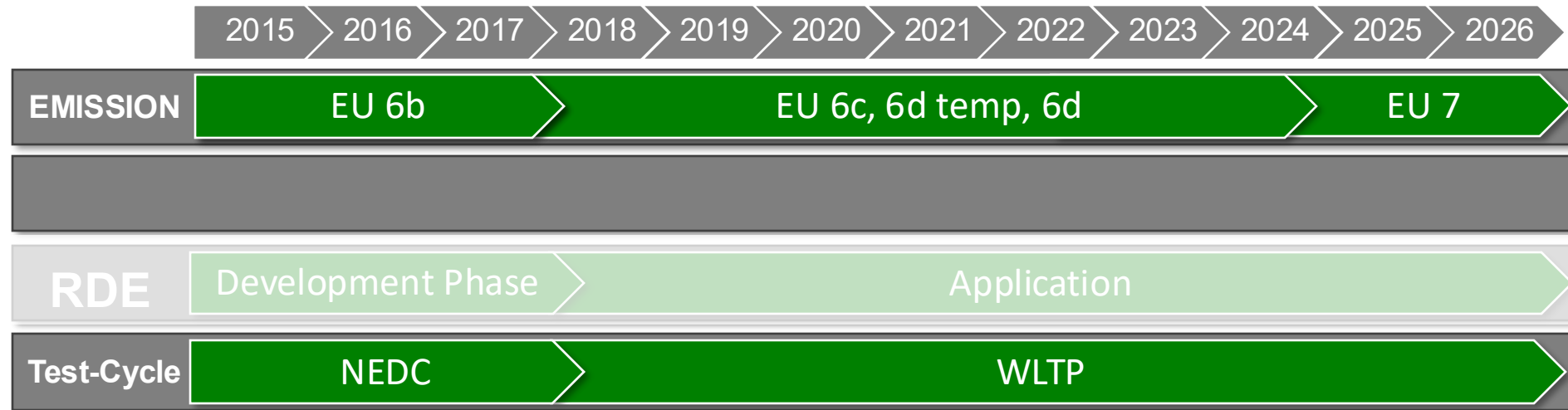
- Propulsion systems and challenges
- State of the art (example passenger cars)
- Possible pathways
- Hybrid powertrain architectures
- Dedicated hybrid engines
- Outlook

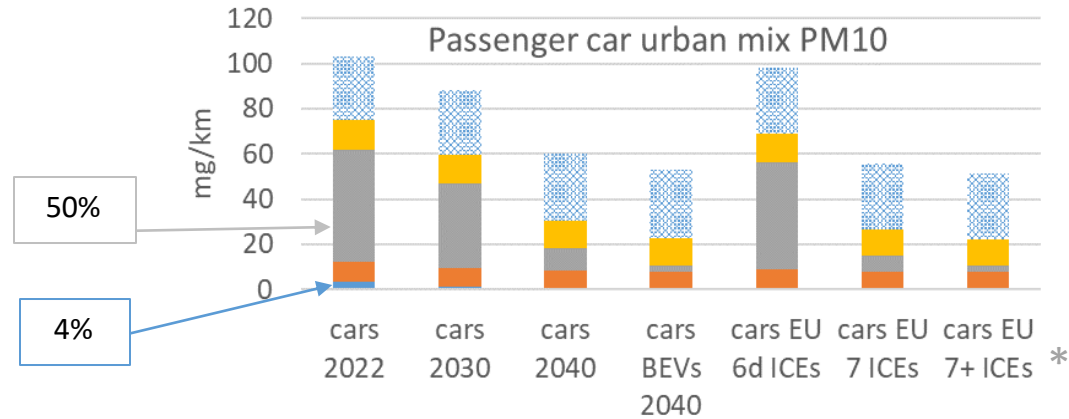


Future Combustion Engines – Motivation and Challenges

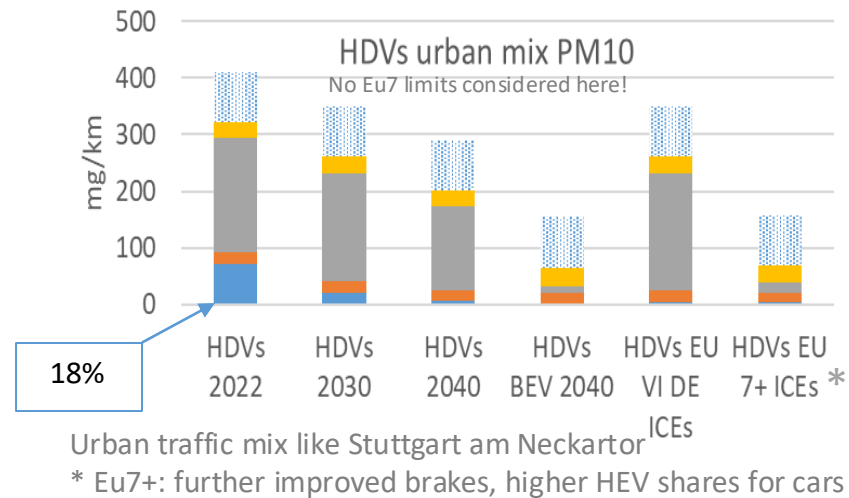


Example: Boundary Conditions for Passenger Cars in Europe





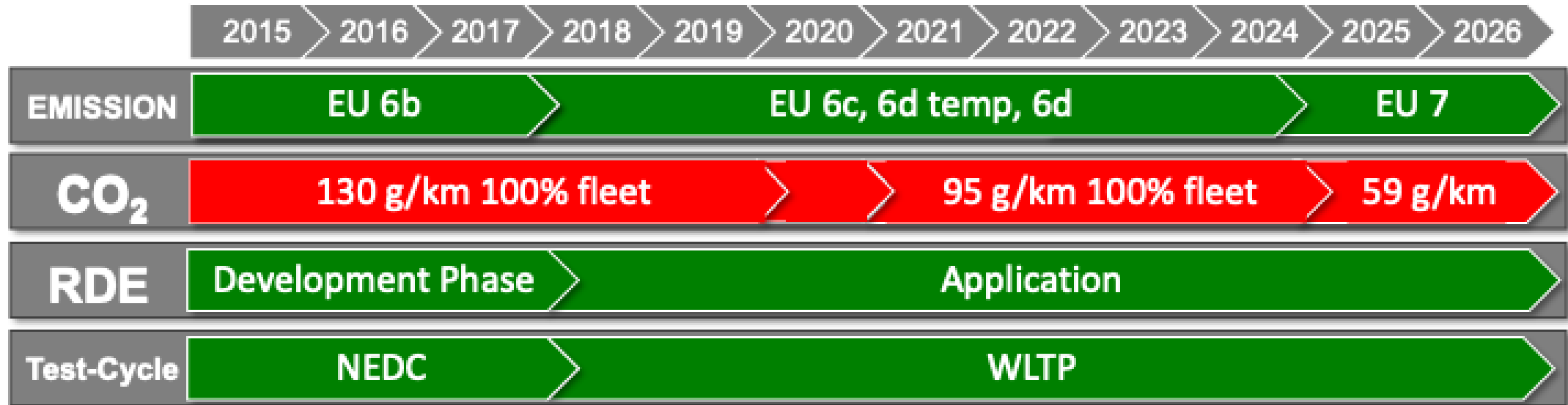
PM10_TP PM10 TyreWear PM10 BrakeWear
PM10 RoadWear PM10 Resusp.



- Exhaust emissions hardly relevant anymore
- BEV, HEV, EU7 ICE have roughly the same PM10 and PM2.5 emissions in total
- Brake wear is currently dominant in urban areas. However, this is significantly reduced by electrification and EURO 7 limits
- Potential for reduction in tire and road abrasion and resuspension currently low
- PM10 air quality limits for 2030 critical

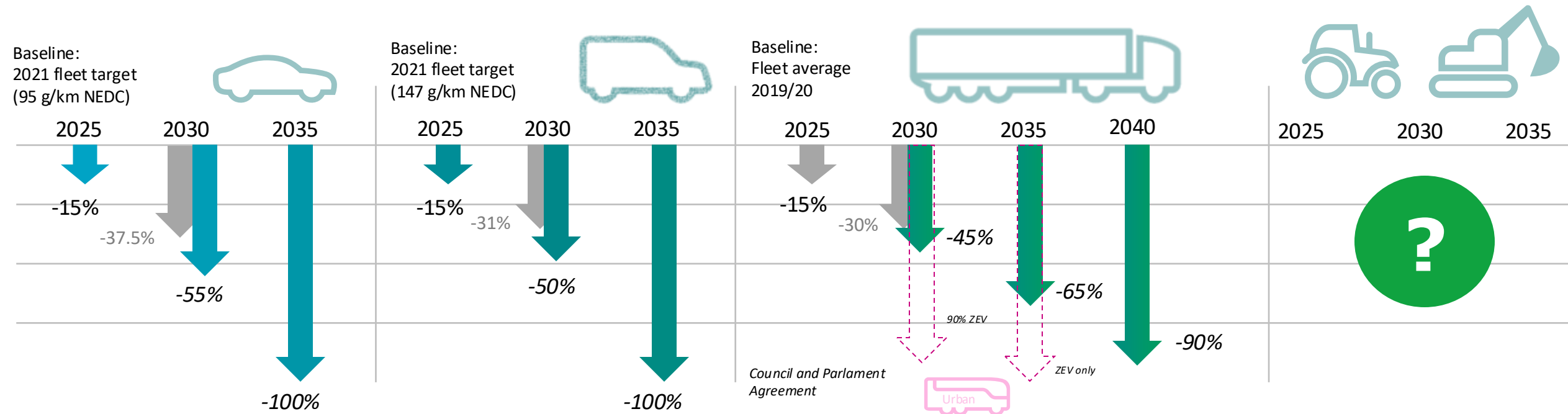
Source: ITnA / Hausberger, 2024

Example: Boundary Conditions for Passenger Cars in Europe



EU CO₂ Standards

Outlook across segments



Accepted ZEV_{CO2}:
BEV, FCEV
H₂-ICE & ICE with E-Fuel ?

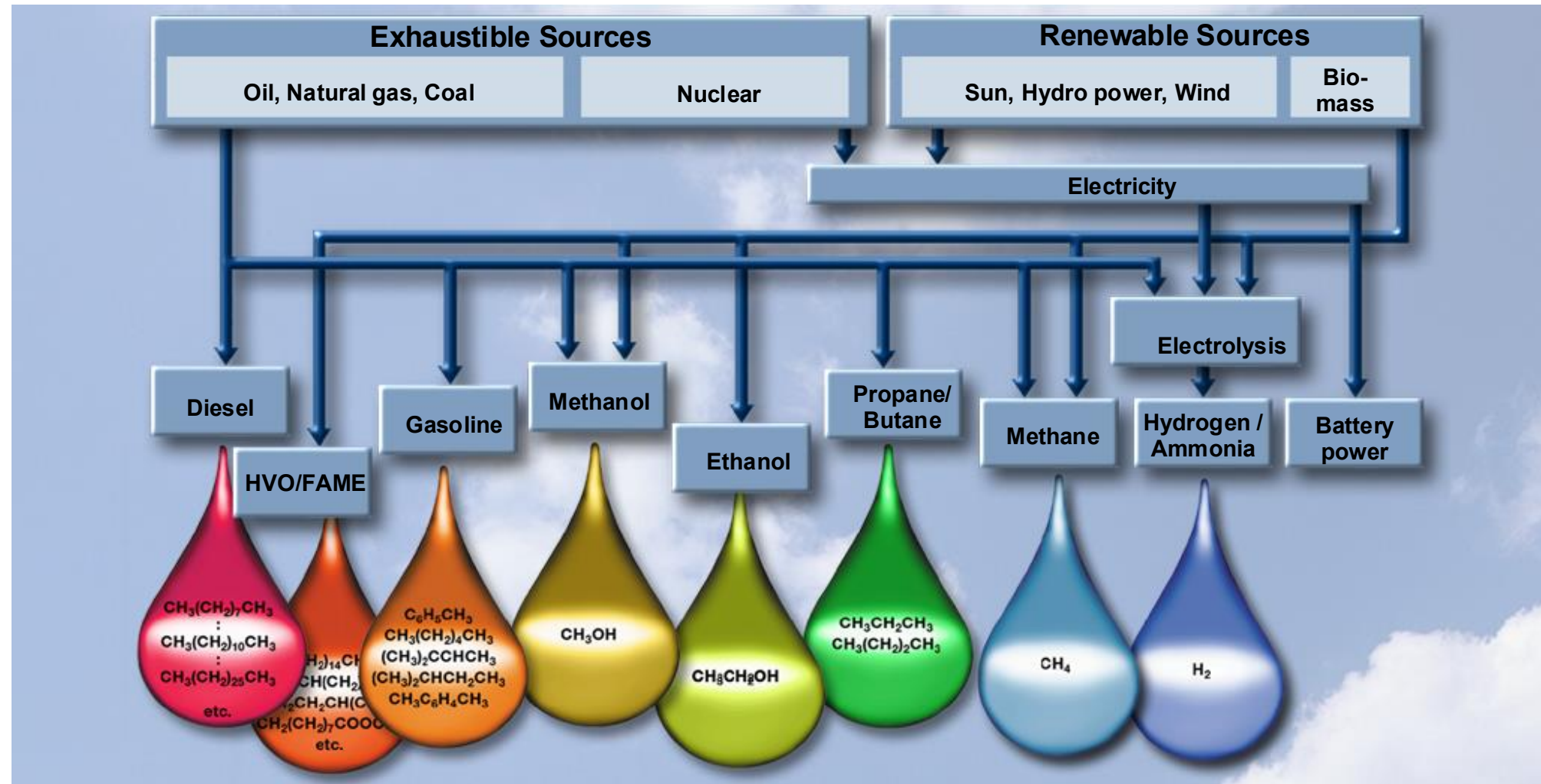
Accepted ZEV_{CO2}:
BEV, FCEV, H₂-ICE*
*ZEV: max. 3 g/(t·km) or 1 g/(p.km)

Potential ZEV_{CO2}:
BEV, FCEV, H₂-ICE
(E-Fuel, Alcohols)

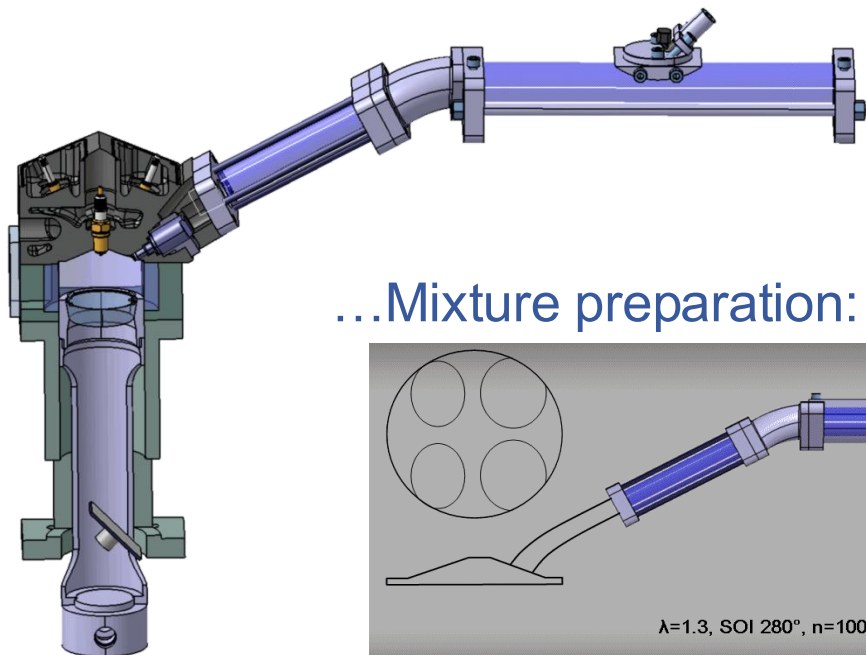
Grey: targets in current regulation. *Italics*: proposed.

Source: AVL / Wieser, 2024

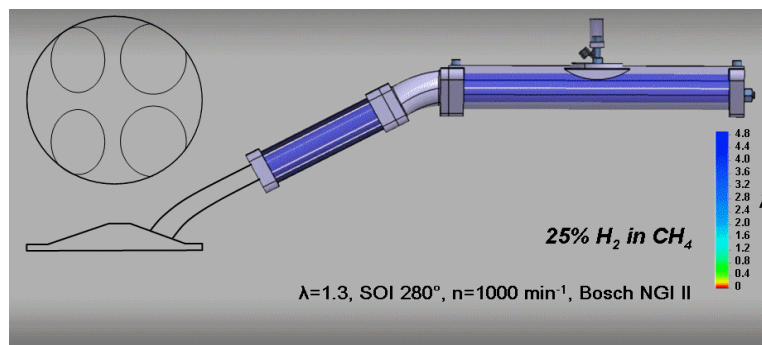
Various forms of Energy and Fuels for propulsion systems



Source: Göschl BMW adapted

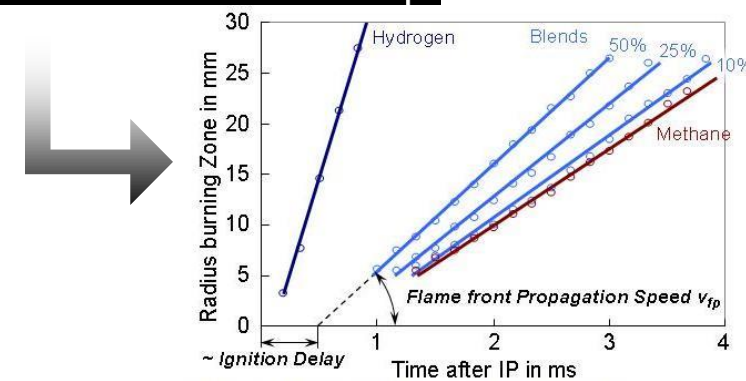
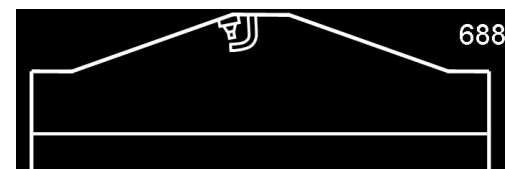


...Mixture preparation:



- Mischungsverhalten, Ladungsschichtung, Einfluss auf Verbrennung & Anomalien

...combustion:



- Kenngrößen der Verbrennung, Beherrschbarkeit, Anomalien, Wirkungsgradpotentiale

Measured Tailpipe Emissions in Transient Cycles

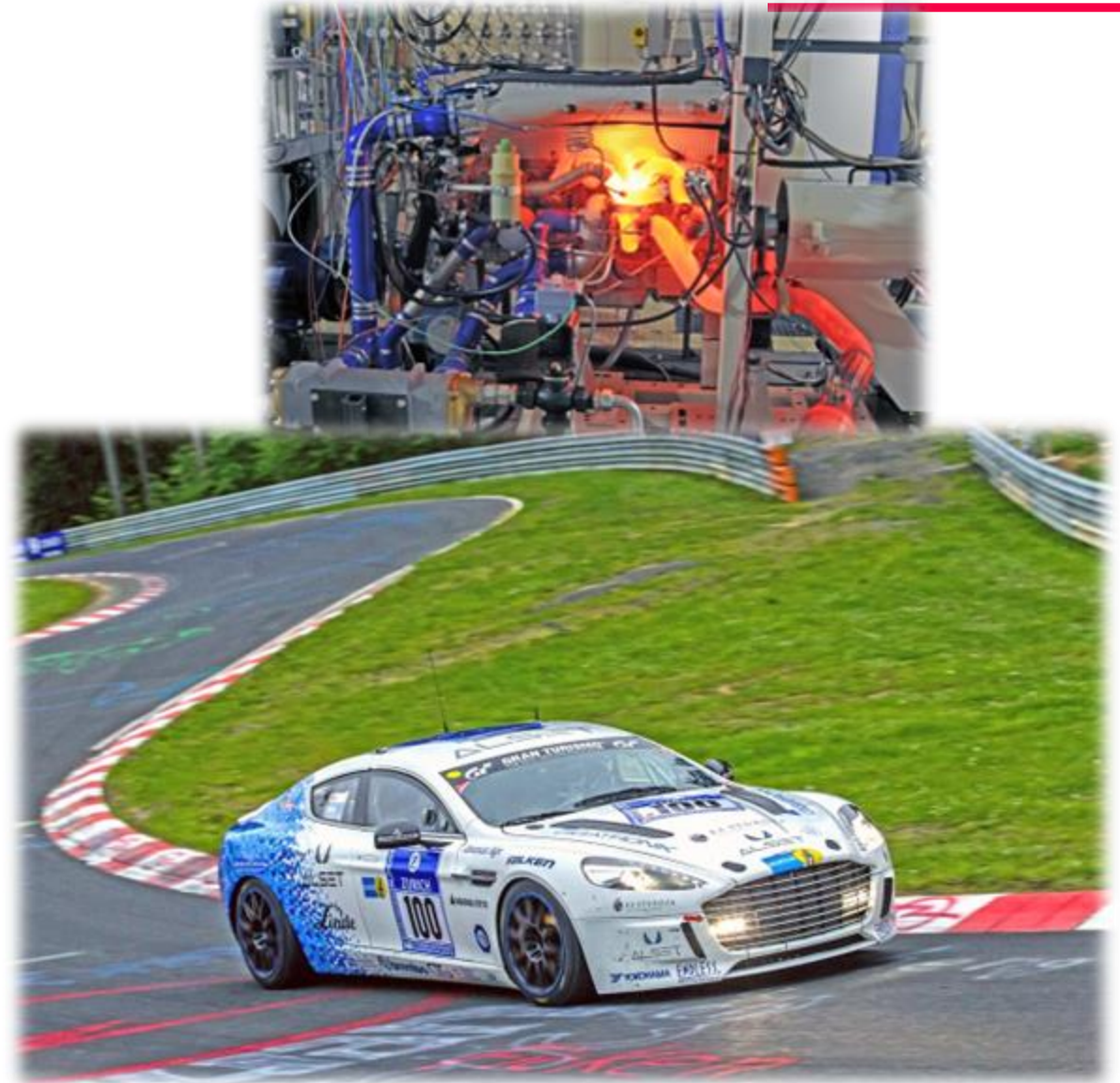
- Very promising results demonstrated on the transient test bed

					
<i>NO_x Tailpipe</i>	1,7 mg/km	26,7 mg/km	280 mg/kWh	22,6 mg/kWh	Stage V 2000 mg/kWh Euro 7 Truck 220 Tier5 220 / 2031 (40/2033)
<i>Test Cycle</i>	WLTC 23°C	ERMES 23°C	WHTC combined	NRTC combined	
<i>Configuration</i>	SCR Late Post Inj.	SCR Early Post Inj.	OC / SCR VNT	OC / SCR VNT	
<i>Engine</i>	2 lit. IL4	2 lit. IL4	13 lit. IL6	13 lit. IL6	

Hydrogen ICE for Aston Martin

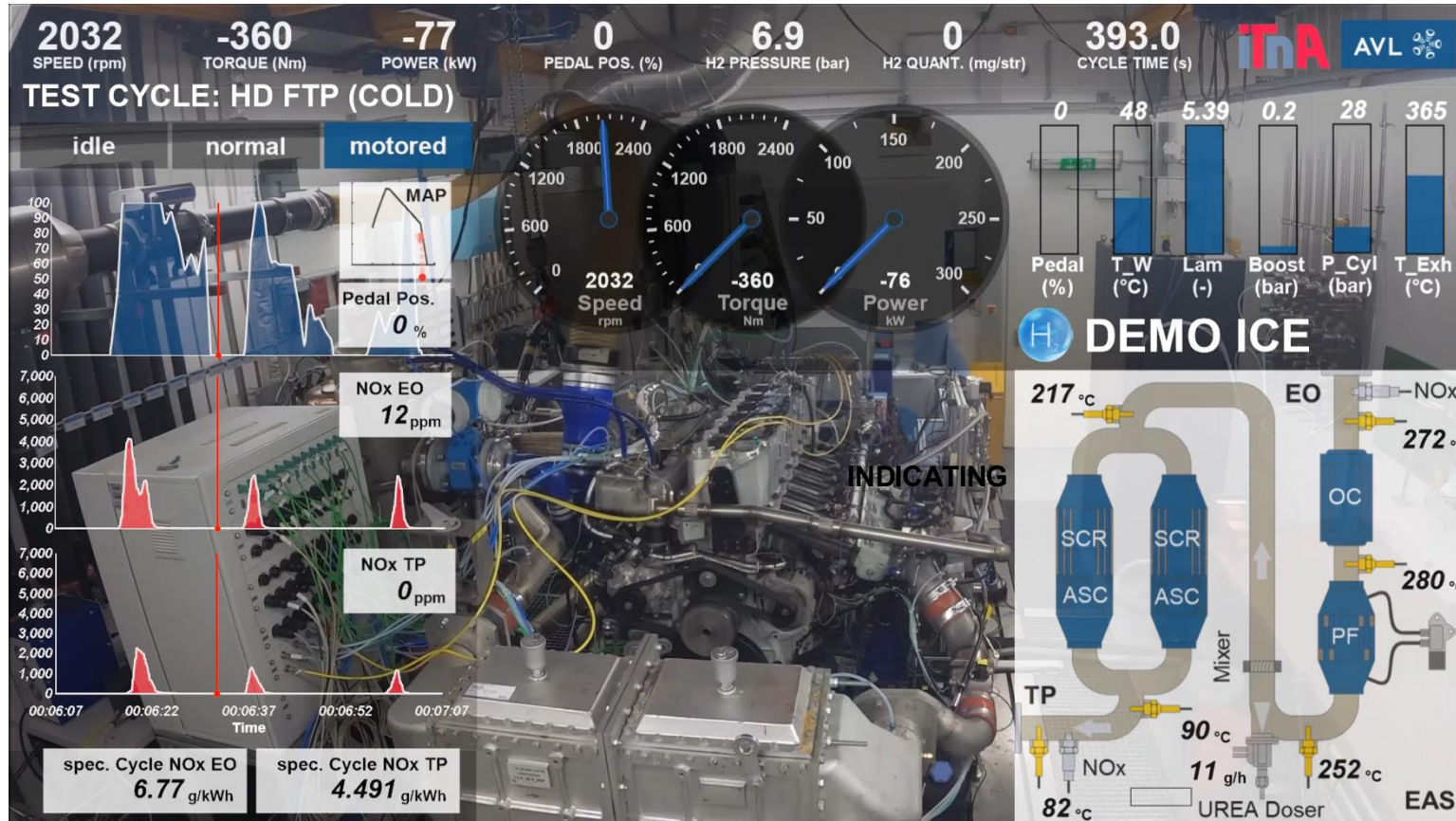
Example for robustness: 24h Race Nürburgring

- Base engine
 - Aston Martin AM11
 - Gasoline NA
 - 6 dm³ capacity
- Race engine
 - Implementation
 - H₂-Injection
 - BiTurbo, AirRestrictor
 - Operation with
 - Hydrogen
 - Gasoline or
 - Mixture of both



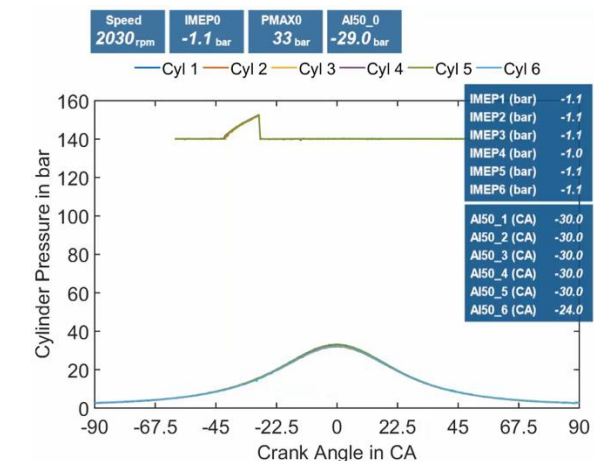
Challenges Hydrogen HD engine

Transient operation (FTP cold)



Source: Schneider ITnA

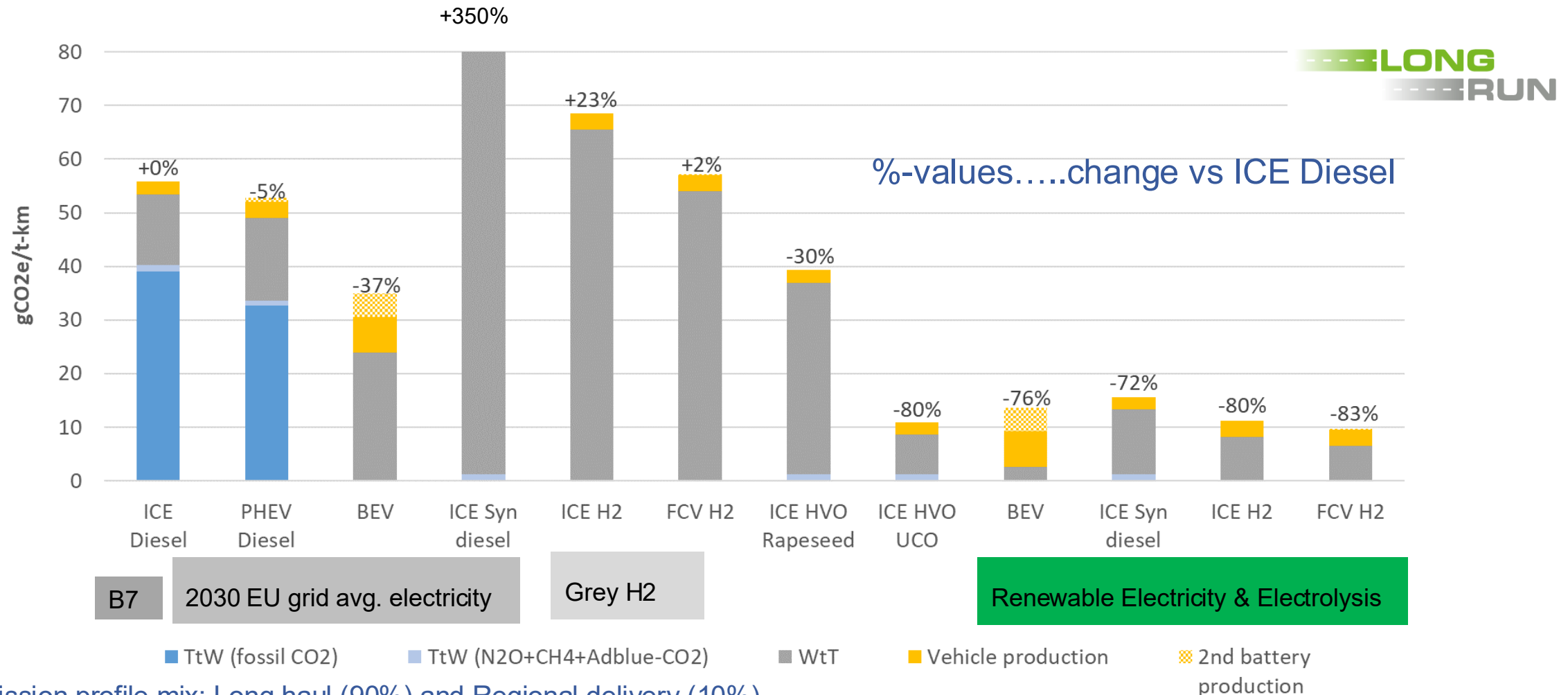
- Pre-ignitions during transient load changes
- Possible triggers
 - Increased residual gas content due to temporary increased exhaust backpressure
 - Enrichment
 - Increased oil combustion after motored or idling operation



Results CO_{2e} (VECTO + LONGRUN LCA for 2030 technologies)

Reference 2030, EU Mix 254 g CO_{2e} / kWh_{el};

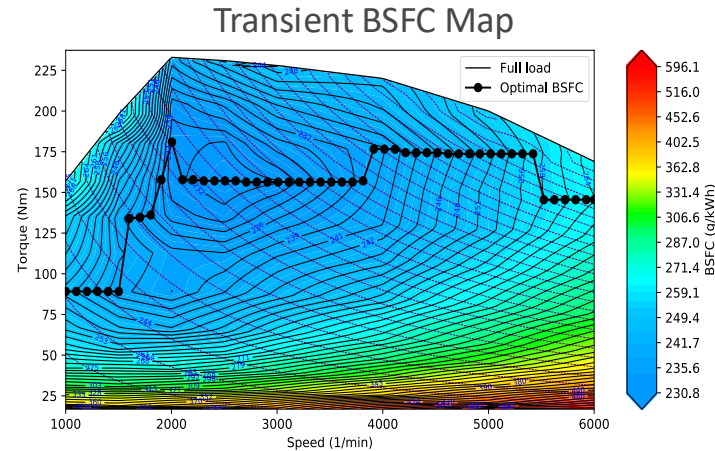
Renewable: 28 g CO_{2e} / kWh_{el}; 1,2 Mio km



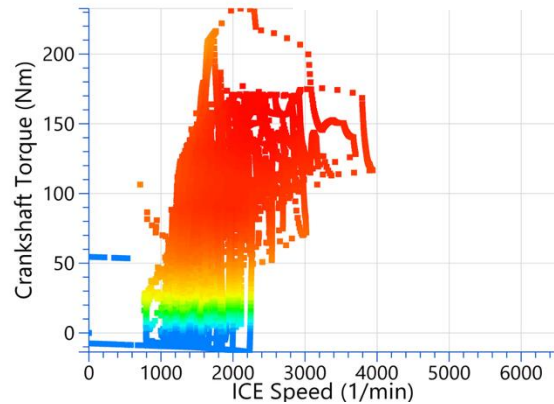
Mission profile mix: Long haul (90%) and Regional delivery (10%)

Source: Hausberger / ITnA 2024

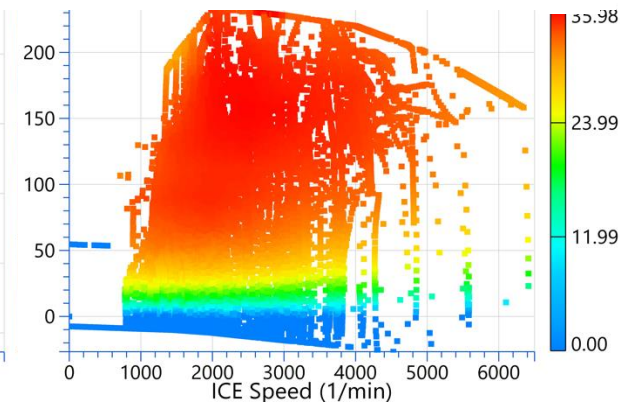
Hybrid powetrains and dedicated hybrid engines using renewable fuel



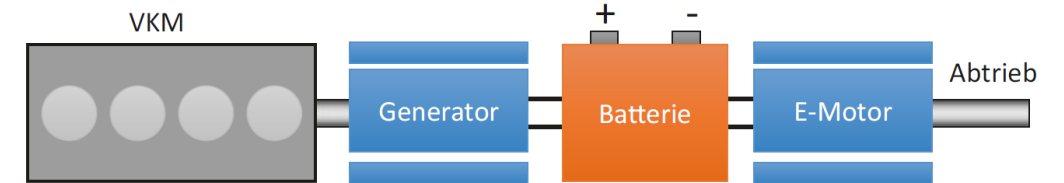
Efficiency WLTC (lab)



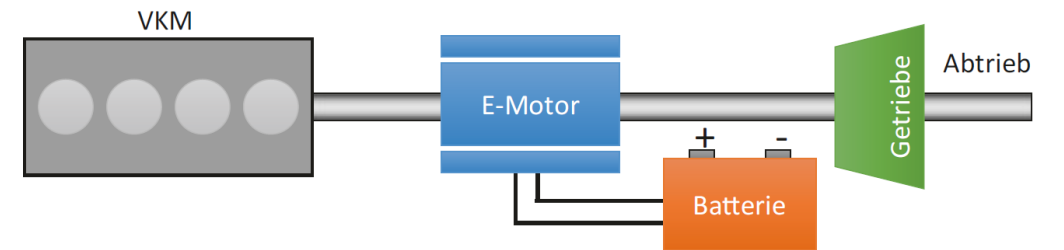
Efficiency rural roads (real world)



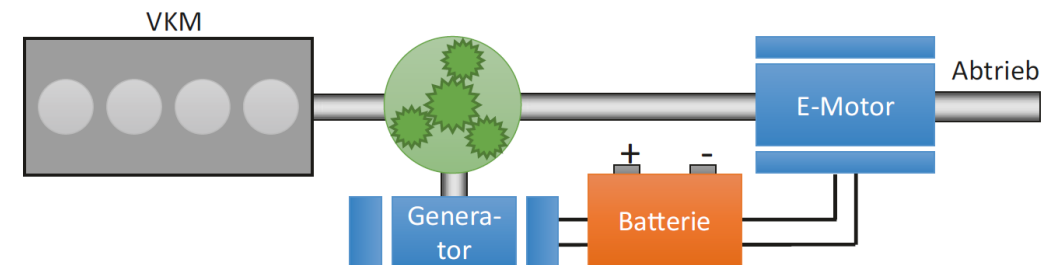
Serial hybrid



Parallel hybrid



Power-split hybrid

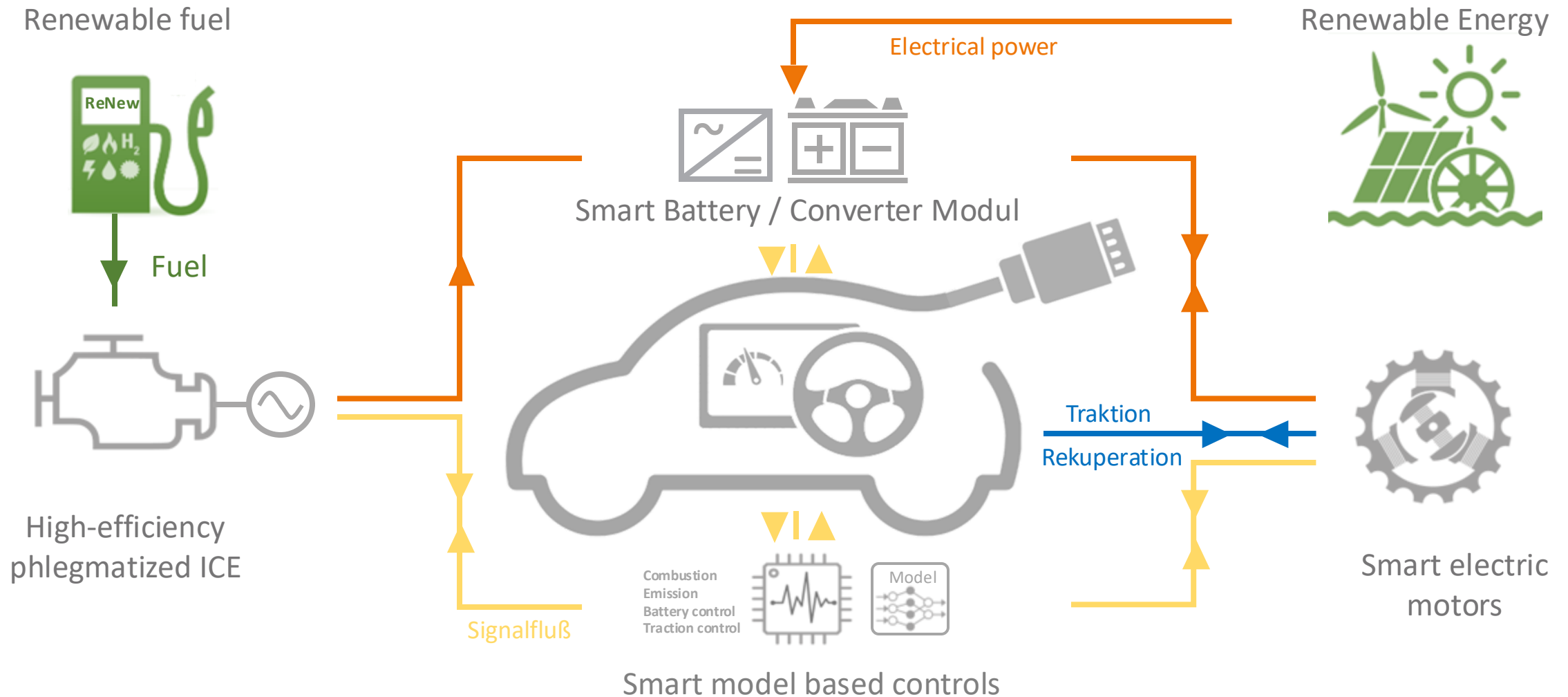


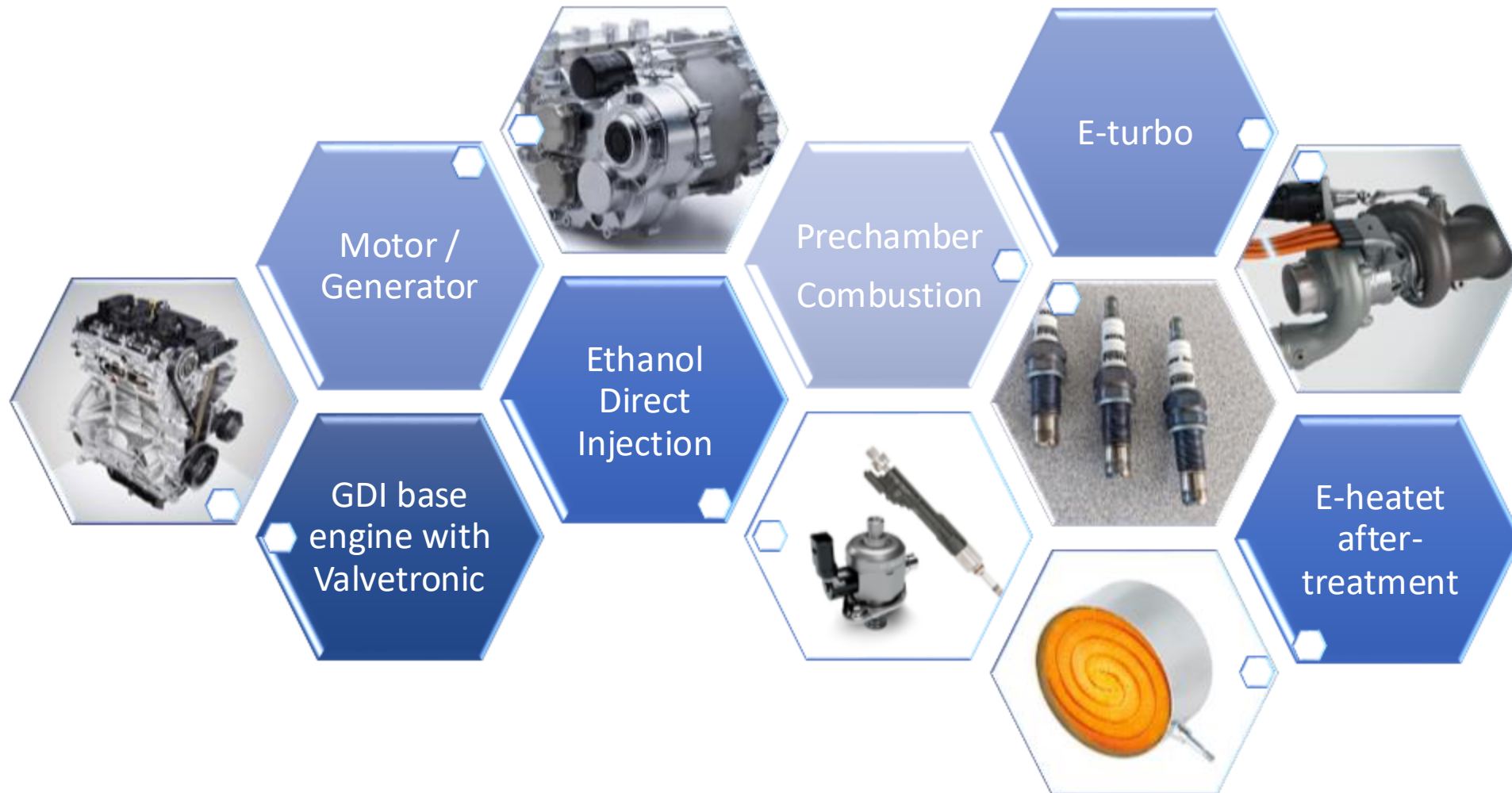
Relevant renewable fuels: Properties

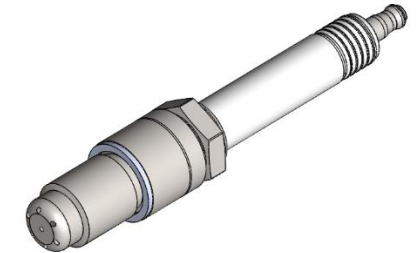
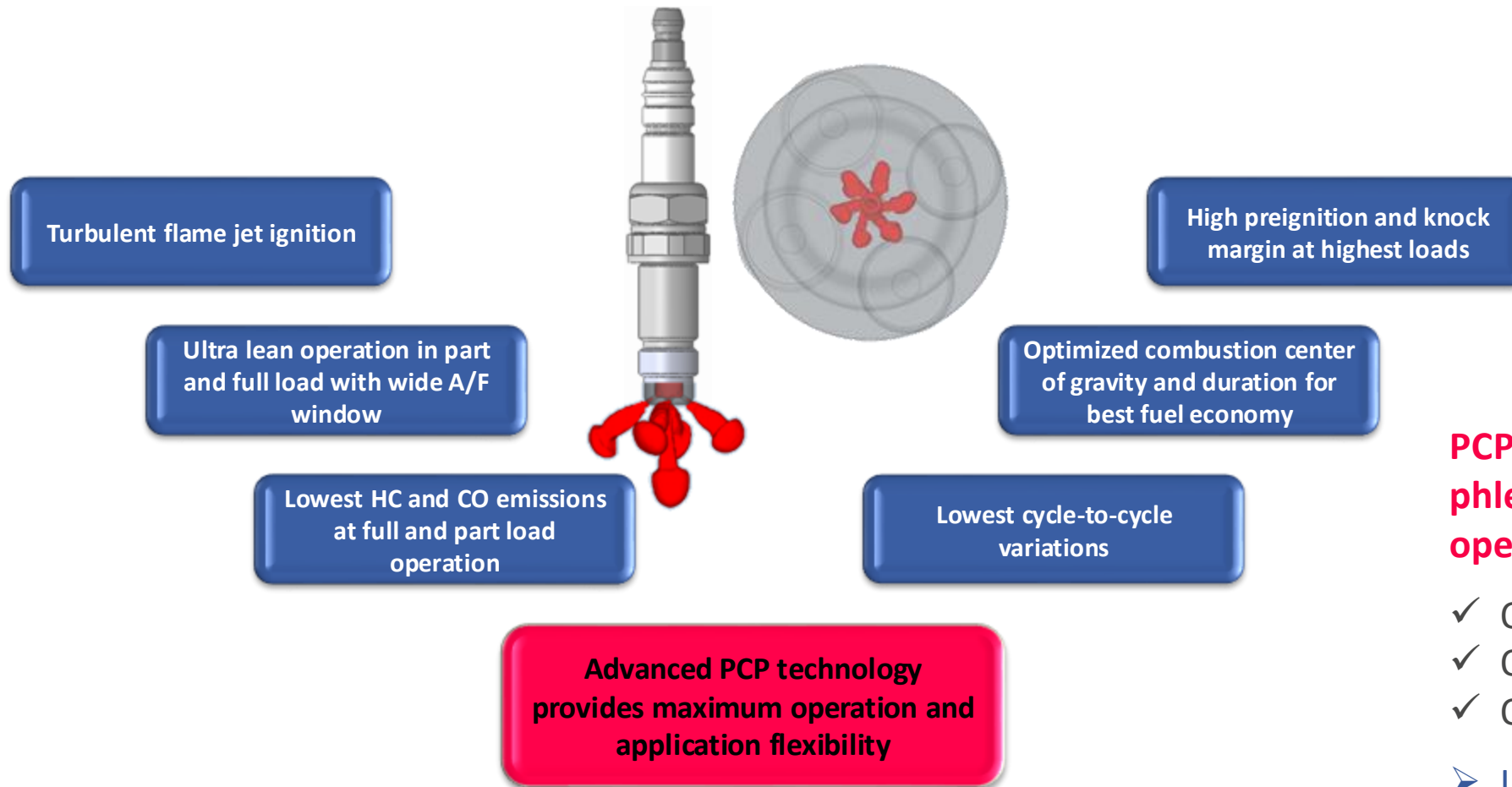


	Unit	Super 95	Methanol	Ethanol	Hydrogen
Calorific value H_u	MJ/kg	42,00	19,70	26,80	120,00
Stoich. air requirement L_{St}	kg/kg	14,50	6,46	9,00	34,20
Heat of Evaporation	kJ/kg	420	1100	910	450
Boiling point	°C	30-190	65	78	-253
Density (15 °C)	kg/m ³	735-785	791	789	0,09
Octane rating RON	-	95,0	116	112	130
Ignition temperature	°C	230-450	455	425	585
Minimum ignition energy	mJ	0,24	0,28	0,28	0,017
Laminar flame speed ($\lambda = 1$)	cm/s	35	40	40	230

Serial hybrid topology & architecture

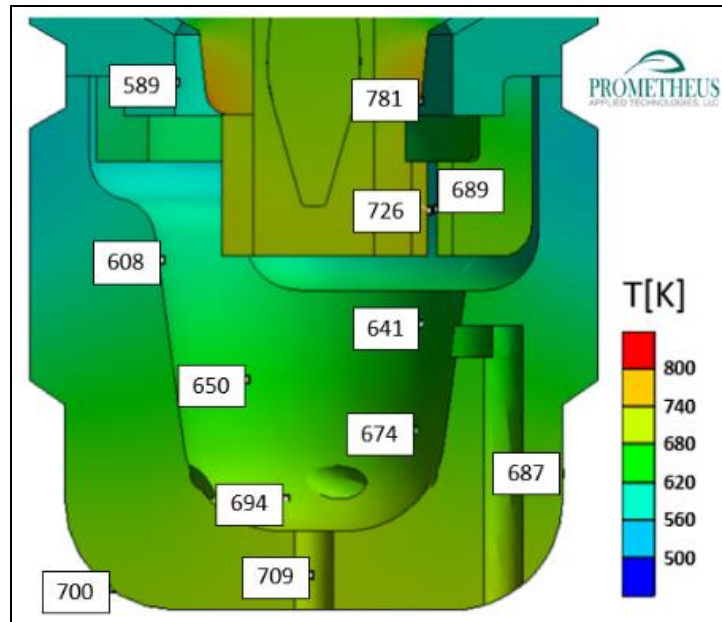






PCP technology is best suited for a phlegmatized engine running WOT operating points:

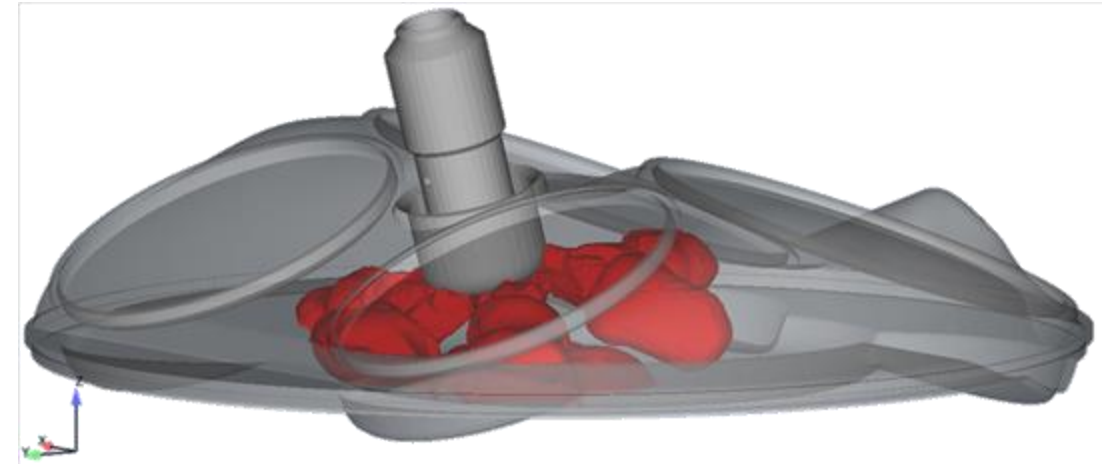
- ✓ Optimal scavenging & filling
- ✓ Optimal thermal management
- ✓ Optimal flame jet orientation
- Ultra low NO_x emissions
- Fast combustion @ 8 °CA MFB50



Thermal management of the PCP

Optimal prechamber and electrode temperatures are required for an extended combustion operating range without knock or preignition at WOT as well as to ensure the longest durability.

- Conjugate heat transfer calculations considering actual cylinder head cooling.
- Modeling of arc travel and arc development in the prechamber

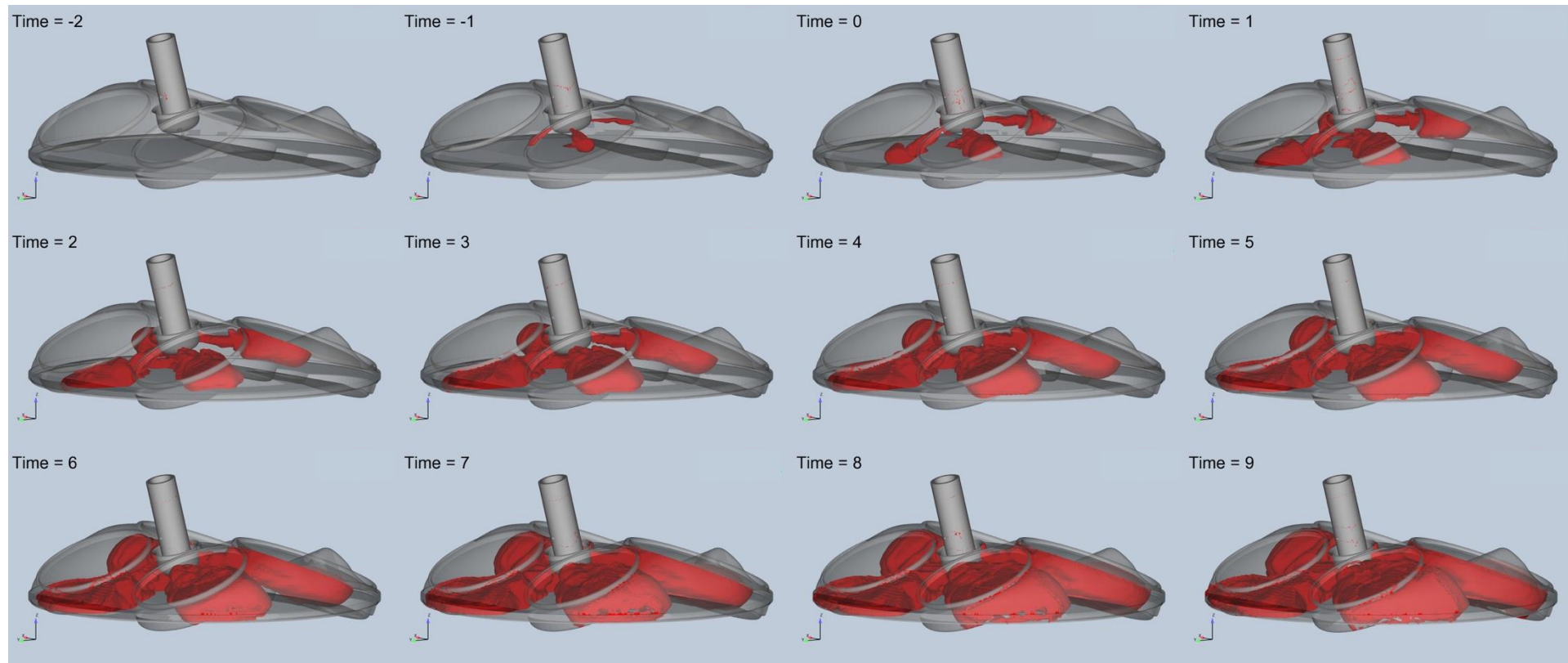


Flame jet orientation and piston geometry

The complete burn of the fuel trapped in the prechamber prior to jet release is key to generating powerful flame jets.

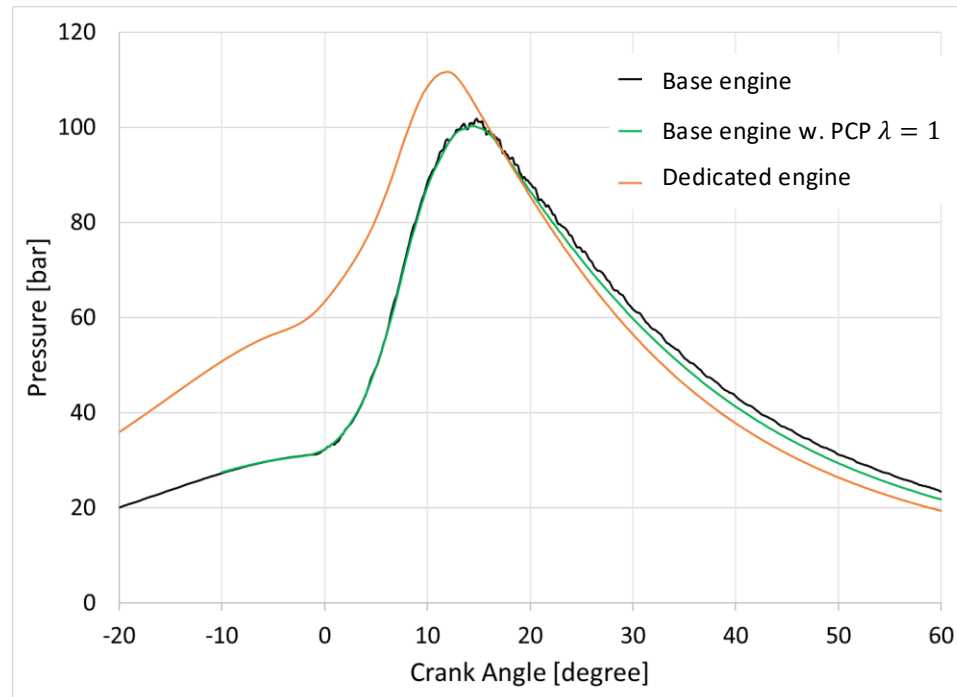
The jet orientation considers the lambda distribution in the main chamber created by residual gas non-uniformity and the injection strategy and geometry.

Very powerful flame jets achieve fast flame propagation with ultra-lean mixture ($\Lambda=1.9$)



(2000 1/min 16 bar BMEP)

Cylinder pressure (2000 1/min 16 bar BMEP)

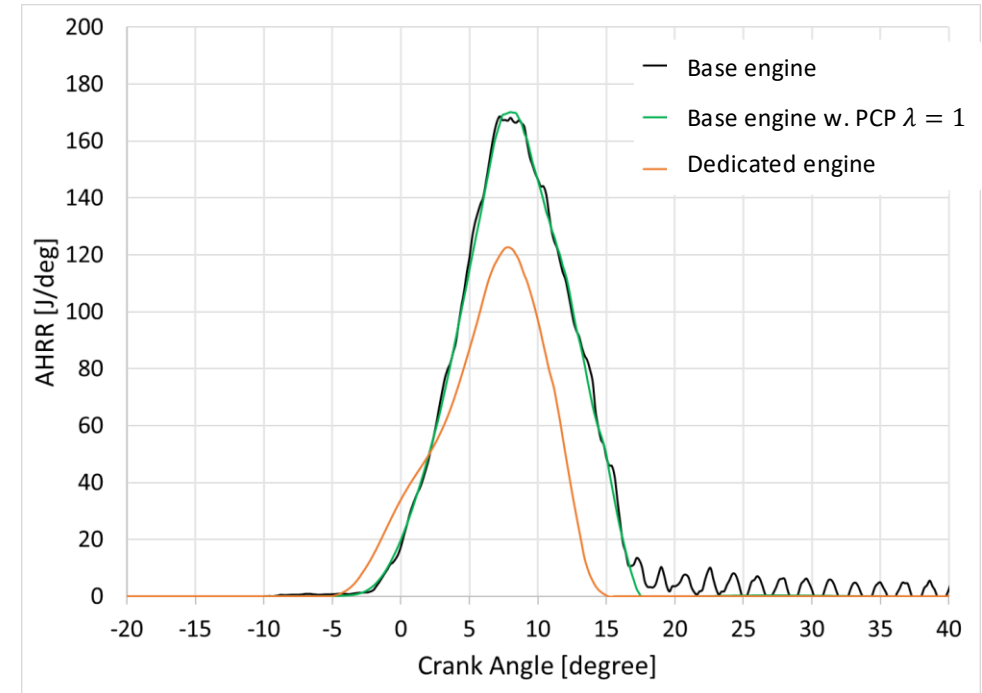


Baseline: 37 % efficiency, 2300 ppm NO_x

Engine compression ratio: 11:1; Mixture Lambda: 1.0

Boost pressure: 1.4bar; Spark Timing: -6 CAD

Heat Release (2000 1/min 16 bar BMEP)



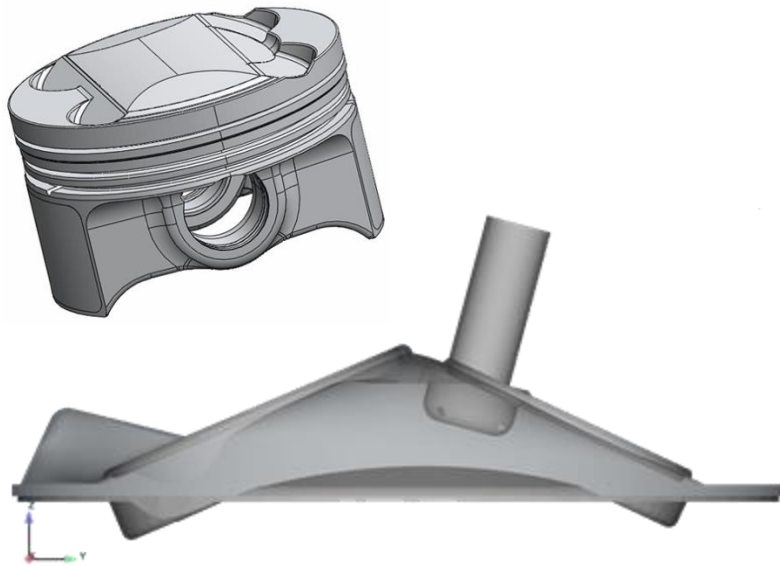
Innovative solution: 45 % efficiency, < 100 ppm NO_x

Engine compression ratio: 13:1; Mixture Lambda: 1.9

Boost pressure: 2.2bar; Spark Timing: -9 CAD

Combustion
Chamber

Power kW	Speed rpm	BMEP bar	BTE %
20	1200	13,3	44
40	2000	16	45
60	3000	16	45



Intelligent Predictive Operating Strategy (PreOps)

- Backend- and map-based prediction of actual power requirements
- Two control levels: Dynamic programming long range and model predictive short range control

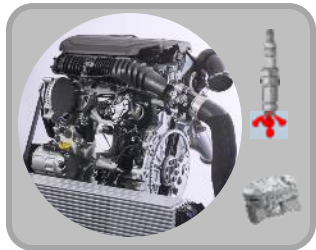
Smart Battery



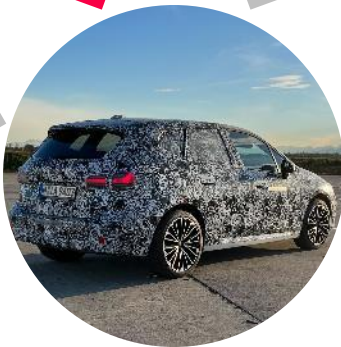
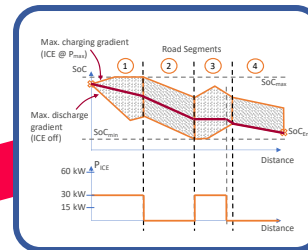
5-phase motor



Prechamber ICE



PreOps



Traction Motor

- In-house developed 5-phase self-excited synchronous motor
- Neodyme free, electrical excitation through harmonics
- 120 kW (30 s) / 80 kW (cont.) allowing $v_{\max}$ 160km/h
- Mech. efficiency between 92,0 - 97,8 %

Battery and Inverter (Step 1)

- Battery: State-of-the-art 400 V Li-Ion
- Inverter: in-house developed multiphase SiC

Phlegmatized internal combustion engine

- 1.5 l, 3 cylinder (based on BMW B38)
- Mech. efficiency up to 44 % @ 100 ppm NO_x
- Ultra-lean, homogenous, prechamber combustion
- Quasi-stationary operation in 3 power levels (20, 40, 60 kW)

Generator – motor

- In-house developed 3 phase permanent magnet synchronous motor
- Mech. efficiency 98,4 %

Brake losses & recu potential

Ø Braking power with conventional ICE:

2.39 kW



Hybridization

Ø Braking power with hybrid powertrain:

352 W

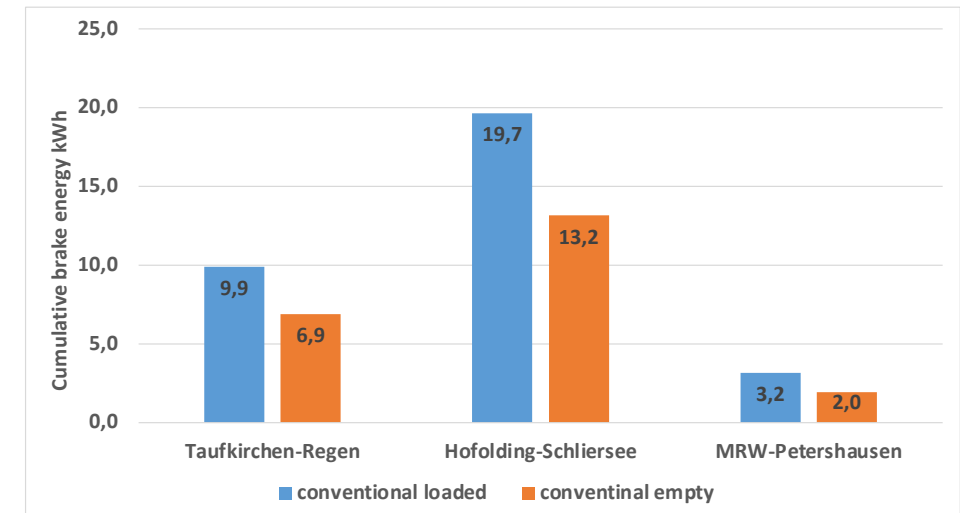
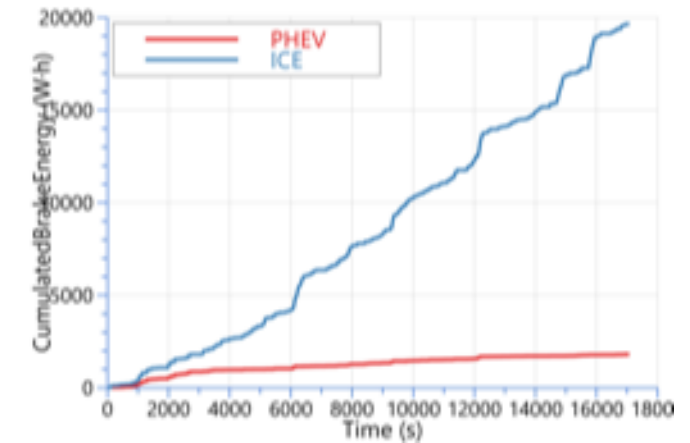
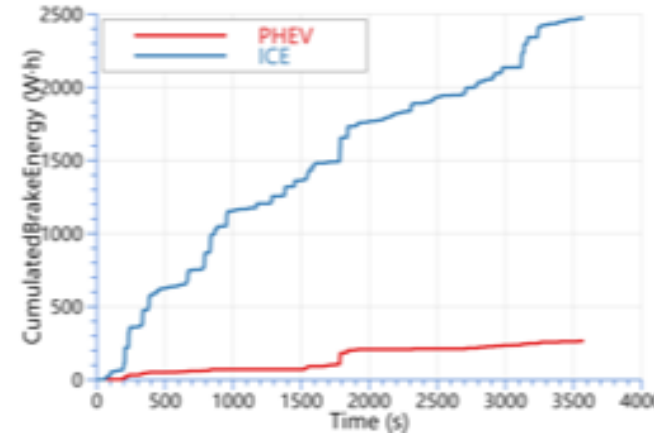


Phlegmatization and hybridization reduce energy dissipation at the brakes by **more than 85 %** (also brake wear!)

Residual brake usage mostly near-standstill (low energetical relevance) or during singular sharp braking maneuvers (high power, not recuperable).

Huge variations in cummulative brake energy due to drive cycle evelvation profile differences.

Brake energy: smooth rural roads



Serial hybrid: virtual driving results

Average ICE & e-motor efficiency

Ø Efficiency with conventional ICE:

32.36 %

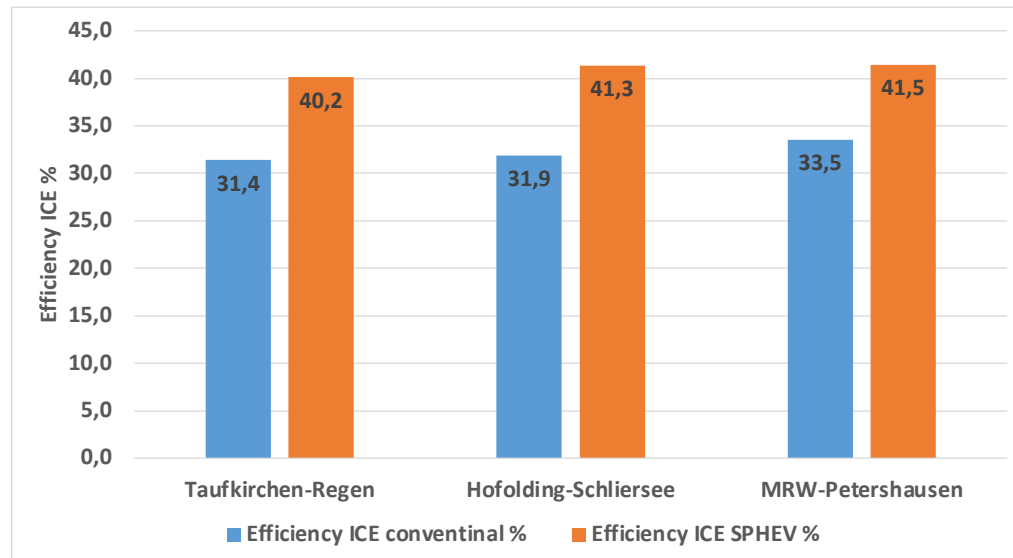


Phlegmatization
Hybridization

Ø Efficiency with phlegmatized ICE:

40.86 %

Low-load, low-efficiency operation is **entirely avoided**.



Ø Efficiency with conventional e-motor:

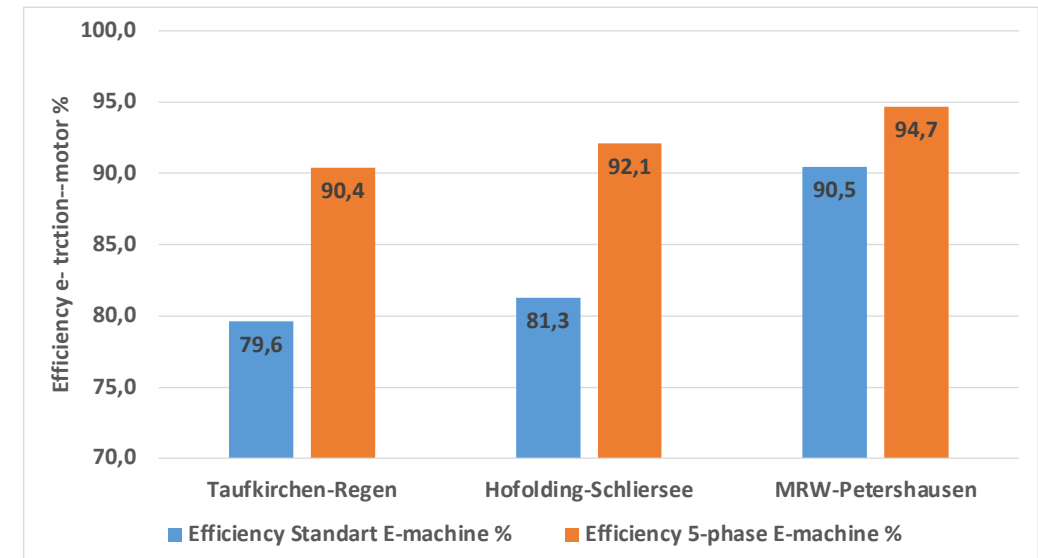
84,8 %



Innovative 5 phase design

Ø Efficiency with innovative e-motor:

92,7 %



Vielen Dank für Ihre Aufmerksamkeit !

